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(71) Applicant(s)

Uponor Limited

(Incorporated in the United Kingdom)

**Hillcote Plant, PO Box 1, Blackwell, NR ALFRETON,
Derbyshire, DE55 5JD, United Kingdom**

(72) Inventor(s)

Jyri Jarvenkyla

Mikael Andersson

David Charles Harget

Eino Holso

(74) Agent and/or Address for Service

Dobb Lupton Broomhead

**Fountain Precinct, Balm Green, SHEFFIELD, S1 1RZ,
United Kingdom**

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(54) Plastics pipe

(57) A plastics pipe which comprises an inner core and an outer protective layer, in which the dimensions of the pipe and the protective layer are such that the ratio of the external diameter of the pipe to the thickness of the protective layer is at least 100, and the cohesive strength of the outer protective layer, excluding any lines of weakness, at least at the ends of the pipe is greater than the strength of the adhesive bond between the outer protective layer and the inner core. The outer layer adjacent the ends of the pipe can be removed when two pipe sections are to be joined by electrofusion welding.

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PLASTICS PIPE

This invention relates to plastics pipes and more particularly to a novel construction of plastics pipe, a method for its manufacture, and a method for making joints in such a pipe.

In the handling, installation and connection of plastics pipes, the pipe surface is easily damaged. In modern plastic pipe installation techniques, for example, a tunnel is bored in the ground for the pipe, and the pipe is then pushed or pulled through the tunnel, for example, into an excavated hole where the next pipe joint is to be made.

15

The pipe-laying method can subject the pipe to substantial bending, tensile and abrasive contact forces. This is disadvantageous since bending, stretching and abrasion of a pipe can result in a deterioration of its mechanical strength. In addition, the useful life of the pipe may be reduced by diffusible materials in the ground, or by environmental conditions.

It will be apparent that the method of pipe-laying can also result in the pipe becoming scratched and dirty. This is disadvantageous firstly as the pipe material may be notch sensitive, in which case any scratches may cause greater damage to occur in the pipe during subsequent

handling or use. Secondly, dirt on the pipe prevents successful welding. At the present time, a common technique for jointing plastic pipes is electric welding, and particularly electrofusion welding, using an electrofusion coupler. The main reason for failure of joints using an electrofusion coupler is that the surface of the pipe is dirty or has become oxidised. For this reason the pipe ends always have to be cleaned and abraded or scraped, for example with sandpaper or a metal scraper, before jointing. In practice, the cleaning and abrading or scraping is often uneven (the underside of the pipe in particular may be treated less carefully) and the quality of the end result depends upon the professional skill of the installer.

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A variety of suggestions have been put forward to overcome the above-mentioned disadvantages.

In European Patent Application No. 0474583 there is described a plastic pipe to be laid in the ground which comprises a gas or water conducting core pipe provided with an outer hose of a thermoplastic material having a higher flexibility than the material of the core pipe. The pipe is stated to be able to resist the extensive mechanical stresses to which it is subjected during direct laying into the ground. It is stated to be easy to remove the outer hose adjacent the ends of the pipe when two pipe sections are to be assembled by welding.

It is also stated that formation of cracks caused by damage to the protective hose does not spread to the core pipe, but stops when the hose has been penetrated.

5 In PCT/FI92/00201 there is described a plastics pipe for making pipe joints characterised in that the pipe is covered by a plastic surface layer as a protective coating which is easily detachable at least at the ends of the pipe, in order to uncover the joint surface of the
10 pipe necessary for making the pipe joint. The protective coating can contain UV stabilisers and may be applied by co-extrusion through a cross-head extrusion nozzle. Various ways of making the protective coating easily detachable from the core pipe are disclosed, including
15 the use of fillers in the coating, the choice of chemically different plastics materials for the coating and the pipe, extruding the coating at low temperatures, and the introduction of adhesion preventing agents.

20 In PCT/FI93/00038 there is described a two-layer plastics pipe which comprises a core pipe whose material, size and structure essentially meet the requirements set by the material to be conveyed and an outer hose provided around the core pipe by a suitable coating method, the
25 properties of the outer hose essentially meeting the requirements set by the environment and for the laying procedure. The stiffness of the outer hose, based on its material properties or the design of the outer hose, is

higher than the stiffness of the core pipe manufactured from the same amount of material, and the outer hose is removable at least at the ends of the pipe. The outer hose is again applied by co-extrusion using a cross-head
5 extrusion die. The protective outer hose is made so as to be easily detachable at least at the pipe ends and to have low adhesion thereto.

The entire disclosures of all the above-mentioned
10 patent specifications are incorporated herein by reference.

The present invention provides a plastics pipe comprising an inner core and an outer protective layer
15 having an improved combination of mechanical and physical properties.

It has now been found, in accordance with one aspect of the invention, that the relative dimensions of the
20 plastics pipe and the thickness of the outer protective layer have a profound effect upon the performance of the pipe. It has also been found that, firstly in order to achieve an advantageous combination of mechanical strength to resist the severe conditions involved in
25 laying the pipe and also to provide a sufficient degree of environmental protection, together with an appropriate degree of peelability, requires a particular choice of mechanical properties and dimensions.

In accordance with a first aspect of the present invention, therefore, there is provided a plastics pipe which comprises an inner core and an outer protective layer, in which:

5

the dimensions of the pipe and the protective layer are such that the ratio of the external diameter of the pipe to the thickness of the protective layer is at least 100, and

10

the cohesive strength of the outer protective layer, excluding any lines of weakness, at least at the ends of the pipe, is greater than the strength of the adhesive bond between the outer protective layer and the inner

15

core.

In accordance with a further aspect of the invention, it has also been found that the extent of the adhesion between the inner core and the outer protective

20 layer also has a substantial influence upon the performance of the pipe. If the adhesion is too great or too small, the mechanical properties of the pipe, and in particular the impact strength, may be adversely affected.

25

The adhesive bond preferably has relatively low peel and relatively high shear characteristics. Preferably the adhesion between the outer protective layer and the

inner core is in the range of from 0.2 to 0.5 N/mm width, measured by a semi-tensile peel test as hereinafter described.

5 Whilst it may be possible to obtain an adhesion between the protective layer and the inner core within the preferred range using a cross-head extrusion method wherein the protective layer is extruded over the solidified inner core, we have found that consistently
10 improved results are obtained by dual extrusion in which both components are extruded and brought together before substantial oxidation of the outer surface of the inner core has taken place.

15 Accordingly, in another aspect the invention provides a method for the production of a plastics pipe comprising an inner core and an outer protective layer which comprises co-extruding molten plastics materials forming the inner core and the outer protective layer
20 from an extruder die, bringing the extrudates together whilst still hot and allowing them to cool, such that, on cooling, the outer protective layer can be peeled from the inner core, at least at the ends of the pipe, to reveal an inner core surface suitable for electrofusion
25 welding.

In a further aspect, the invention also provides a method of making a joint in a plastics pipe according to

the invention which comprises peeling the outer protective layer from the ends of the pipe to be joined, installing an electrofusion coupler over the bared ends of the pipe and activating the electrofusion coupler to
5 fuse the ends of the pipe thereto.

The plastics pipe can comprise any suitable thermoplastic polymeric material, and particularly suitable polymeric materials include, for example,
10 olefinically-unsaturated polymers and co-polymers, for example, polyolefins such as polyethylene, polypropylene and polybutene, ethylene and propylene co-polymers, for example, ethylene-vinyl acetate polymers, and propylene-vinyl acetate polymers, halogenated-vinyl polymers such
15 as vinyl chloride polymers and co-polymers, polyamides, for example, nylon 6 and nylon 66, and ionomer polymers such as Surlyn.

The inner core of the pipe is chosen to be
20 compatible with the particular application, and in particular with the fluid material to be conveyed by the pipe. For many applications polyethylene is the preferred material for the inner core. The grade of polyethylene chosen, that is to say, high density, medium
25 density, low density or linear low density, will depend upon the particular application. Suitable grades of polyethylene include, for example, Statoil 930 (natural), Neste NCPE 2600 (natural) and Neste NCPE 2467 BL and NCPE

2418. Any suitable equivalent grade of polyethylene may of course also be used.

An advantage of the plastics pipes of the present invention is that the normal UV stabiliser and colorant package need not be included in the plastics material of the inner core, provided that sufficient quantities of these materials are included in the outer protective layer. This enables the inner core to comprise natural polymeric material, free or substantially free from additives which add to the cost of the core material and which, in certain circumstances, may impair the mechanical or physical properties of the core material.

The outer protective layer is preferably formed from a polymeric material having good mechanical and physical properties, together with an ability to receive quantities of stabilising materials, in particular UV stabilisers, sufficient to protect the inner core.

Preferred polymeric material for the outer protective layer comprise propylene homo- and co-polymers, and especially propylene co-polymers such as, for example, Neste SA 4020G. Other polymeric materials with suitable mechanical and physical properties, for example nylons and Surlyn, can also be used in appropriate circumstances.

Suitable stabiliser materials include, for example, titanium dioxide, carbon black, and other fillers. Whilst carbon black is an excellent UV stabiliser and reinforcing filler, buried pipes are frequently colour-coded and its use is therefore not possible for many applications. Titanium dioxide is, therefore, the preferred filler and UV stabiliser, since this is also compatible with many colorant packages. Other filler materials such as chalk and talc, and those mentioned in PCT/F193/00038 may also be used. The preferred filler particle size will depend on the filler being used, but for titanium dioxide, for example, the average particle size range is preferably from 0.003 to 0.025 μ m.

A particularly preferred plastics pipe according to the present invention comprises an inner core of polyethylene and an outer protective layer of a propylene co-polymer. The pipe can of course comprise more than two layers of polymeric material, provided that at least one inner core and one protective outer layer are present.

Whilst the thickness of the outer protective layer needs to be sufficient to accept the appropriate quantities of UV stabilisers and colourants necessary to protect the inner core and also to provide appropriate identification, if it is too thick, rendering the outer

layer too stiff, we have found that the impact strength of the pipe is unexpectedly reduced.

Without wishing to be bound by any particular theory, it is believed that the impact strength of the plastic pipes of the invention is related in part to the adhesion between the inner core and the outer protective layer. If the adhesion is too small the outer protective layer behaves as a relatively thin structurally independent tube and is therefore susceptible to impact damage. If the adhesion is too great, cracks formed by rupture of the outer layer have a tendency to propagate through to the inner core. Ideally, therefore, the adhesion between the outer protective layer and the inner core should be sufficient that, even if the outer core is ruptured and a crack formed, the crack is arrested at the outer layer/inner core interface.

Preferably the outer protective layer has a thickness greater than 0.1mm, more preferably greater than 0.2mm, and most preferably has a thickness in the range of from 0.3 - 0.5mm.

The dimensions of the pipe and the protective layer are such that the ratio of the external diameter of the pipe to the thickness of the protective layer is at least 100. From this it can be seen that it is possible to use a thicker protective layer on a pipe of greater diameter,

although for easy peelability the thickness is preferably kept to a minimum.

5 Examples of suitable pipe external diameters and outer protective layer thicknesses are as follows:

<u>Pipe OD (mm)</u>	<u>Outer layer thickness (mm)</u>	<u>SDR</u>
30 - 50	0.3	100 - 166
63 - 125	0.4	157 - 312
>125	0.5	250 - 500 (at 10 250mm Pipe OD)

15 Preferably the dimensions of the pipe and the protective layer are such that the ratio of the external diameter of the pipe to the thickness of the protective layer (standard dimension ratio SDR) is in the range of 150 to 400.

It is important, when stripping off the outer protective layer from the ends of the pipe, that the cohesive strength of the outer protective layer is greater than the strength of the adhesive bond between the outer protective layer and the inner core. The reason for this is to prevent any substantial sized particles of the outer protective layer from adhering to the outer surface of the inner core and interfering with the jointing process, when using, for example, an electrofusion coupler. Preferably the arrangement is such that when stripped off, the outer protective layer leaves no residue on the outer surface of the inner core.

In general, the cohesive strength of the outer protective layer is preferably at least 5MPa, and most preferably in the range of from 5MPa to 10MPa.

5 Notwithstanding the above, the outer protective layer may be provided with lines of weakness to assist peeling back, which lines may be produced by scoring, or preferably by suitably shaping the extrusion die, or by cooling the die locally, for example, as described in
10 PCT/F192/00201.

 In order further to assist the stripping off the outer protective layer, the extrusion conditions may be arranged such that the strength properties of the outer
15 protective layer are different in the radial and axial directions.

 As previously mentioned, the adhesion between the outer protective layer and the inner core is preferably
20 in the range of from 0.2 to 0.5 N/mm width as measured by a semi-tensile peel test. A suitable test is described below:

 A test specimen of pipe is prepared by cutting two
25 parallel axial notches through the whole of the surface layer for 50mm, and extending these notches for a further 50mm with a depth such that 0.3mm is left of the surface

layer. A further 20mm length of specimen is allowed before the vertical alignment with the load cell.

The tear test is performed in an Instron model 1197 with a speed of 100 mm per minute. The pipe is placed so that the start of the tearing at the beginning of the through notch depth is 120 mm from the centre of the load cell and the distance from the start of the tearing to the fastening point of the load cell is 750 mm. The apparatus is shown diagrammatically in figure 1. The result is that the largest tear angle is achieved whilst tearing that part of the pipe with a notch through the surface layer.

Although not presently preferred, it may be possible to provide an adhesive layer between the inner core and the outer protective layer which would have the appropriate adhesion characteristics. If an adhesive is used it should preferably have a high cohesive strength so that it does not leave a residue when stripped from the pipe, or alternatively, if any residue is left on the pipe it should be such as to aid, rather than hamper, fusion.

As previously mentioned, the plastics pipe of the present invention is preferably produced by co-extrusion, for example, from an extruder die connected to a twin barrel, twin screw extruder, or connected to two

individual extruders, the die being fed with separate streams of molten plastics material. Preferably the melt streams are brought together in the die, that is to say, the materials are brought together in the pressure area of the die and exit as a single extrudate. Alternatively, the die may be provided with concentric die outlets fed with the separate streams of molten plastics material which are to form the inner core and the outer protective layer. In this case, the extrudates, on leaving the extruder die outlets, can be brought into contact with each other in a sizing die which simultaneously adjusts the outer diameter of the pipe. The extrudates are preferably brought into contact with each other at a point close to the extruder die outlet, in order to avoid any substantial oxidation of the surface of the inner core. For example, with extrudates travelling at a speed of 1 metre per minute, the sizing die is preferably not further than 15cm from the extruder die outlet.

Whilst it may in certain circumstances be possible to pass the inner core extrudate through an individual sizing die before applying the outer protective layer this is not preferred because it has been found that the sizing die creates an outer surface layer on the inner core which is more susceptible to degradation, possibly due to induced shear orientation or shear nucleation in the outer surface which contacts the sizing die.

The temperature of the extrudates will depend upon the nature of the polymeric material, but, for example, using a polyethylene inner core and a propylene co-polymer outer protective layer the temperature of the extrudate at the die outlet is preferably from 180 to 220°C. Preferably the temperature of the extrudates when they are brought together is at least 150°C, most preferably from 180 to 220°C.

The method of the invention can consistently produce an inner core and an outer protective layer having an adhesion within the preferred range, and by an appropriate choice of the material of the outer protective layer it can be arranged that the outer protective layer can be peeled from the inner core without leaving any significant residue on the surface of the inner core. If necessary, the physical properties of the outer protective layer can be adjusted by the addition of more or less fillers and other additives. A preferred polymeric material for the outer protective layer comprises, for example, propylene co-polymer comprising from 1 to 6% by weight, based upon the total weight of the composition, of a filler such as titanium dioxide. Preferably the outer protective layer has a tensile strength of from 15 to 25MPa.

In general we have found that it is preferable not to use low molecular weight additives such as, for

example, processing aids, in the method of the invention. However stearates, for example, calcium stearate, have been found to be effective as processing aids without substantially adversely affecting the adhesion between
5 the inner core and the protective layer.

Antioxidants can be included in the formulation of the protective layer as required. If appropriate, they can be omitted from the formulation of the inner core
10 provided that suitable quantities are included in the outer protective layer.

The invention is illustrated by the following
Example:

15

EXAMPLE

A number of formulations for the inner core and the outer protective layer were made up with compositions as
20 set out in Table 1. The formulations were extruded using a main extruder and a smaller additional extruder provided with concentric die feed. The melt streams were merged prior to exit from the hot dies. In one experiment, the extrudate, having a diameter of 80mm, was
25 passed through a sizing die of diameter 66.8mm to give a dual layer pipe of external diameter 63.8mm, outer protective layer thickness 0.3mm and inner core thickness

6.2mm. In another experiment, a dual layer pipe of 40mm external diameter was extruded.

Samples of the 40mm OD pipes were subjected to the semi-tensile peel test previously described, and the results are given in Table 2. Table 3 shows similar results on samples which could not be peeled at room temperature and therefore were heat treated in an oven before being subjected to the peel test. These examples are included for comparison purposes.

Samples of the tubes were also subjected to ageing according to the weather durability test of ISO 4892. The test method is given below. The properties of the pipes were found to be substantially unaffected after being subjected to the ageing test showing that the natural inner core was effectively protected by the stabiliser package included in the outer protective layer. The results are given in Table 4.

Further samples of the pipes were subjected to B50 impact testing in accordance with CEN TC155W1 081(291) document ref. 155N696E. The impact tests were performed at 0°C and -20°C.

It was found that pipes with a polypropylene co-polymer outer layer passed all the impact tests and had

approximately the same behaviour as uncoated polyethylene pipe of the same diameter.

Pipes with a polypropylene homopolymer outer layer
5 had reduced impact strength of 33Nm at 0°C compared with more than 150 Nm for an equivalent uncoated polyethylene pipe.

A 50/50 polypropylene homopolymer and co-polymer
10 mixture was also tested. This pipe passed the impact test at 0°C but the results at -20°C were the same as for the polypropylene homopolymer.

Failure in the impact test was due to a type of
15 rupture in which a crack originated in the outer layer and propagated to the pipe. It is believed that those samples which failed the impact test did so because the adhesion between the outer layer and the inner core was too great.

20

The reader's attention is directed to all papers and documents which are filed concurrently with or previous to this specification in connection with this application and which are open to public inspection with this
25 specification, and the contents of all such papers and documents are incorporated herein by reference.

All of the features disclosed in this specification (including any accompanying claims, abstract and drawings), and/or all of the steps of any method or process so disclosed, may be combined in any combination, except combinations where at least some of such features and/or steps are mutually exclusive.

Each feature disclosed in this specification (including any accompanying claims, abstract and drawings), may be replaced by alternative features serving the same, equivalent or similar purpose, unless expressly stated otherwise. Thus, unless expressly stated otherwise, each feature disclosed is one example only of a generic series of equivalent or similar features.

The invention is not restricted to the details of the foregoing embodiments. This invention extends to any novel one, or any novel combination, of the features disclosed in this specification (including any accompanying claims, abstract and drawings), or to any novel one, or any novel combination, of the steps of any method or process so disclosed.

TABLE 1

	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112
Material Pipe	930	930	930	2600	2600	2600	2600	2600	2600	2600	2600	2467b1	2467b1	2467b1	2467b1	2410
Material Skin	1	2	3	1	1	1	1	1	1	1	1	1	1	1	3	1
Master- batch	4	4	4	4	5	5	4	4	4	4	4	4	4	NONE	NONE	NONE
Loading &	10	10	10	10	10	15	15	15	10	0	15					

Material

Two different types of pigmented master batches were used at two concentrations.

- 1 - Polypropylene SA 4020 G manufactured by Neste
 - 2 - Polypropylene SA 4020 G/VA4020 E 50/50 mixture
 - 3 - Polypropylene VA 4020 E
 - 4 - 84571-2009 from Wilson colour tio based
 - 5 - 84671-2100 from Wilson Colour titanate based
- 930 Polyethylene Statoil 930 (natural)
 2600 Polyethylene Neste 2600 (natural)
 2467b1 Polyethylene Neste N2410

Master Batches

	845671-2009	84671-2100
TiO ₂	30	2,5
Irganox 1010	1	1
Chiasorb 944	1	1
Titanate	0	approx 30
PP(mf1 5.0)	carrier	carrier

TABLE 2

Prod. No.	Surface Layer		1. Notch through N/mm	2. Notch with 0,3 mm left N/mm	3. Force to break N/mm	Remark
	thickn. mm	width mm				
E101	0,34	10,03	1,25	4,88	5,23*	1. & 3. Came off well, big tension.
	0,35	9,88	1,16	5,36	5,66	2. Came off well at notch through the surface layer.
	0,41	9,75	1,38	7,38	5,74*	Was torn at the side of the notch with 0,3mm left.
E102	0,31	9,80	1,30	2,75	5,39*	1. Came off well, big tension.
	0,40	9,94	1,08	2,51	7,40*	2. Came off well, big tension.
	0,30	9,80	1,71	2,24	6,12*	3. Came off well, big tension.
E103	0,30	9,70	2,52	3,91	7,19*	1. Came off well, big tension.
	0,35	10,00	1,40	5,88	-----	2. Break while tearing notch with 0,3mm left.
	0,44	9,50	2,05	4,73	8,47*	3. Came off well, big tension.
E104	0,57	9,75	2,36	7,18	11,84*	1. Came off well, big tension.
	0,51	9,71	0,51	4,22	12,20*	2. Came off well, big tension.
	0,39	9,45	1,00	5,71	10,10*	3. Came off well, big tension.

E105	0,27	9,70	1,39	5,92	6,08*	1. Came off well at notch through the surface layer. Was torn at the side of the notch with 0,3mm left. 2. Break while tearing notch with 0,3 mm left. 3. Came off well.
E106	0,21	10,12	1,53	5,18br	5,18	
	0,26	9,62	2,49	5,87	6,82	
	1,00	9,25	1,45	8,00	20,32	1. Came off well.
E107	0,60	9,80	0	3,77	13,09	2. & 3. Came off without any load at notch through the surface layer.
	0,65	9,50	0	3,63	14,08	
	0,65	10,00	0	4,10	14,0*	1. & 2. Came off without any load at notch through the surface layer, big tension.
	0,65	9,40	0	3,98	13,51	
	1.00	9,30	0,75	8,17	18.80	3. Came off well.

* Maximum force at the tensile test, but there was no break.

TABLE 3

Prod. No.	Surface Layer		1. Notch through N/mm	2. Notch with 0.3 mm left N/mm	3. Force to break N/mm	Remark
	thicken. mm	width mm				
E 97 50°C 1h	0.25	9.75	2.20	2.87	5.12*	1. Came off well, the tearing kept on to the edge of the test piece.
	0.35	10.00	2.40	3.40	6.58*	2. Came off well, the tearing kept on to the edge of the test piece.
	0.25	9.40	2.39	4.36	4.65*	3. Came off well, big tension.
E 97 60°C 1h	0.20	9.40	2.37	2.92	5.87*	1. Came off well, the tearing kept on to the edge of the test piece.
	0.25	9.55	2.25	2.93	5.03*	2. Came off well, big tension.
	0.30	9.65	2.11	3.00	6.79*	3. Came off well, the tearing kept on to the edge of the test piece.
E 97 70°C 1h	0.30	9.80	1.56	3.91	6.36*	1. Came off well, the tearing kept on to the edge of the test piece.
	0.25	9.65	2.33	5.88	6.53*	2. Came off well, the tearing kept on to the edge of the test piece.
	0.25	9.50	2.15	4.73	4.89*	3. Came off well, big tension.
E 100 50°C 1h	0.40	9.55	1.62	4.50	8.64*	1. Came off well, big tension.
	0.43	9.75	1.23	2.61	7.67*	2. Came off well, the tearing kept on to the edge of the test piece.
	0.30	9.75	1.74	2.71	5.74*	3. Came off well, big tension.
E 100 60°C 1h	0.30	9.60	1.82	2.97	5.52*	1. Came off well, big tension.
	0.40	9.75	2.26	4.11	8.07*	2. Came off well, big tension.
	0.25	9.55	2.72	3.56	6.70*	3. Came off well, big tension.
E 100 70°C 1h	0.35	9.90	1.96	3.24	6.97*	1. Came off well, big tension.
	0.30	9.60	2.76	4.37	7.50*	2. Came off well, the tearing kept on to the edge of the test piece.
	0.30	9.50	2.00	3.16	5.63*	3. Came off well, big tension.

* Maximum force at the tensile test, but there was no break.

AGEING OF POLYETHYLENE/POLYPROPYLENE PIPES

Weather-durability Testing According to ISO 4892

Test Object

61 pieces of polyethene pipes with a length of 465mm and a diameter of 40mm

9 pieces, yellow tubes marked E100

9"- E102

9"- E103

9"- E104

8"- E106

8 pieces, white"- E107

9 pieces, black/orange, "- E108

Test Performance

The polyethene tubes were exposed in an Atlas Type 65 Weather-o-meter® according to the rain cycle 102/18.

The temperature on a black standard thermometer was $63 \pm 3^{\circ}\text{C}$ and the relative humidity $50 \pm 5\%$.

The light source was filtrated to reach a lower limit of 290nm.

The irradiance was $61 \pm 6\text{W/m}^2$ in the bandpass 280 - 400nm.

The exposure was completed after 250 hours, which corresponds to a 3 months of light dose in the UV visible wavelength interval (280 - 800nm) for London, England.

TABLE 4

TENSILE STRENGTH SKIN/TESTING INFLUENCE OF UV AGEING										
UV aged	Av tensile str (mpa)		29,53		26,98	27,82	30,74		28,32	
	Variation (%)		1,20		1,30	1,60	2,60		0,80	
	Elongation (%) average		413		368	507	173		120	
	Elong min		400		5,4??	480	20		0	
	Elong max		420		580	540	100		280	
Ref	Av tensile str (mpa)		27,26		26,33	32,17	28,24		28,99	
	Variation (%)		3,80		0,40	5,80			2,30	
	Elongation (%) average		706		540	153	507		453	
	Elong min		700		540	200	500		140	
	Elong max		720		540	400	520		640	
TENSILE STRENGTH SKIN/TESTING INFLUENCE OF UV AGEING										
UV aged	Av tensile str (mpa)		24,40		24,49	24,61	25,24		26,10	
	Variation (%)		0,90		0,50	0,70			7,40	
	Elongation (%) average		673		650	673	673		680	

	Elong min		640		640	660	640	660
	Elong max		720		680	680	700	720
Ref	AV tensile str(mpa)		24,35		24,45	24,79	25,17	25,37
	Variation (%)		1,10		1,80	0,50	0,70	0,50
	Elongation (%) average		673		690	667	685	645
	Elong min		640		640	640	660	600
	Elong max		740		740	720	700	680

CLAIMS

1. A plastics pipe which comprises an inner core and an outer protective layer, in which
5 the dimensions of the pipe and the protective layer are such that the ratio of the external diameter of the pipe to the thickness of the protective layer is at least 100, and
10 the cohesive strength of the outer protective layer, excluding any lines of weakness, at least at the ends of the pipe is greater than the strength of the adhesive bond between the outer protective layer and the inner core.
- 15 2. A plastics pipe according to Claim 1, in which the adhesion between the outer protective layer and the inner core is in the range of from 0.2 to 0.5 N/mm width, measured by a semi-tensile peel test as
20 hereinbefore described.
3. A plastics pipe according to Claim 1 or 2, in which the inner core comprises polyethylene.
4. A plastics pipe according to any of the preceding
25 Claims, in which the outer protective layer comprises a propylene homo- or co-polymer.

5. A plastics pipe according to any of Claims 1 to 4,
in which the inner core is substantially free from
anti-oxidants and/or UV stabilisers.
- 5 6. A plastics pipe according to any of the preceding
Claims, in which the outer protective layer
comprises titanium dioxide filler.
- 10 7. A plastics pipe according to any of the preceding
Claims, in which the out protective layer has a
thickness in the range of from 0.3 to 0.5mm.
- 15 8. A plastics pipe according to any of the preceding
Claims, in which the ratio of the external diameter
of the pipe to the thickness of the protective layer
is in the range of 150 to 400.
- 20 9. A plastics pipe according to any of the preceding
Claims, in which the cohesive strength of the outer
protective layer is in the range of from 15MPa to
25MPa.
- 25 10. A plastics according to any of the preceding Claims,
in which the outer protective layer has a tensile
strength of from 5MPa to 10MPa.
11. A plastics pipe according to any of the preceding
Claims substantially as described in the Example.

12. A plastics pipe substantially as hereinbefore described.
13. A method for the production of a plastics pipe comprising an inner core and an outer protective layer which comprises co-extruding molten plastics materials forming the inner core and the outer protective layer from an extruder die, bringing the molten plastics materials together whilst still hot and allowing them to cool, such that, on cooling, the outer protective layer can be peeled from the inner core, at least at the ends of the pipe, to reveal an inner core surface suitable for electrofusion welding.
14. A process according to Claim 13, in which the inner core comprises polyethylene and the outer protective layer comprises a propylene homo or co-polymer.
15. A process according to Claim 13 or 14, in which the molten plastics materials are brought into contact with each other in the pressure area of an extruder die.
16. A process according to any of Claims 13 to 15, in which the inner core and the outer protective layer are brought together at a temperature of from 150 to 220°C.

17. A process according to any of Claims 13 to 16 substantially as described in the Example.

5 18. A process according to any of Claims 13 to 17 substantially as hereinbefore described.

10 19. A method of making a joint in plastics pipe according to any of Claims 1 to 12 which comprises peeling the outer protective layer from the ends of the pipe to be joined, installing an electrofusion coupler over the bared ends of the pipe and activating the electrofusion couplers to fuse the ends of the pipe thereto.

Relevant Technical Fields

- (i) UK Cl (Ed.N) F2P (PC20, PM1)
(ii) Int Cl (Ed.6) F16L 9/12, 9/133, 11/00, 57/00

Search Examiner
R F PHAROAH

Date of completion of Search
2 MAY 1995

Databases (see below)

(i) UK Patent Office collections of GB, EP, WO and US patent specifications.

Documents considered relevant following a search in respect of Claims :-
1-12, 19

(ii)

Categories of documents

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A: Document indicating technological background and/or state of the art. &: Member of the same patent family; corresponding document.

Category	Identity of document and relevant passages	Relevant to claim(s)
X	GB 2032333 A (E I DU PONT) see page 3, lines 70-100	1, 4
X	EP 0044668 A1 (T P ENGEL) see page 17, line 22; page 19, lines 7-9	1

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